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Mixed μ Robust Finite Word Length Controller Design

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Fragility Problem

- Control system designed by maximising its robustness to plant uncertainty alone may exhibit poor stability margin with respect to controller coefficient perturbation
- Two types of finite word length errors in controller implementation are:
 - Rounding errors that occur in arithmetic operations, and
 - Controller parameter representation errors

These two types of errors are typically investigated separately for mathematical tractability

 We consider second type of FWL errors, which has critically influence on close-loop stability

Existing Approaches

- Two strategies for considering FWL controller parameter representation errors
 - Indirect approach: search for an "optimal" realisation of the given controller that is most robust to FWL errors
 - Direct approach: design controller realisation by considering both robust control criteria and FWL errors
- In literature, direct approach is also referred to as non-fragile, defragile or resilient control
 - Some works assume controller parameter perturbation block is 2-norm bounded
 - More realistic ones assume parameter perturbation is independent and magnitude bounded
- Yang *et al.* [20] design robust FWL H₂ controller by considering all vertices of FWL perturbation hypercube

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Our Contributions

With similar hypothesis to Yang *et al.* [20], we study robust FWL $\rm H_{\infty}$ output feedback controller, and our contributions are

- FWL robust control performance measure is proposed, which takes into account robust control requirements and FWL effects on controller implementation
- Robust FWL controller design problem is naturally formulated as a mixed μ problem which can be solved effectively with the aid of mixed μ theory
- Our proposed method is computationally more attractive than Yang *et al.* [20]

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Plant Model

- Plant is described by known nominal model P̂_g(w) and unknown but bounded structured uncertainty Û(w), where w ∈ C
- $\hat{\mathbf{P}}_{g}(w)$ is given as

 $\mathbf{x}_{P}(k) \in \mathbb{R}^{n}$: state, $\mathbf{v}(k) \in \mathbb{R}^{n_{1}}$: uncertainty-linked input, $\mathbf{w}(k) \in \mathbb{R}^{n_{2}}$: external disturbance input, $\mathbf{u}_{P}(k) \in \mathbb{R}^{s}$: control input, $\mathbf{h}(k) \in \mathbb{R}^{n_{1}}$: uncertainty-linked output, $\mathbf{z}(k) \in \mathbb{R}^{n_{2}}$: controlled output, $\mathbf{y}_{P}(k) \in \mathbb{R}^{t}$: measured output

• $\hat{\mathbf{P}}_{g}(w)$ connects with $\hat{\mathbf{U}}(w)$ through **h** and **v**

$$\mathbf{v} = \hat{\mathbf{U}}(w)\mathbf{h}$$

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Structured Uncertainty

• Unknown structured uncertainty $\hat{\mathbf{U}}(w)$ takes the form

$$\hat{\mathbf{U}}(w) = \operatorname{diag}\left(\hat{\mathbf{U}}_1(w), \cdots, \hat{\mathbf{U}}_{b+d}(w)\right)$$

where $\hat{\mathbf{U}}_{i}(w) = \varphi_{i}(w)\mathbf{I}_{p_{i}}$ with $\varphi_{i}(w) \in \mathbb{C}, \forall w \in \mathbb{C}, \forall i \in \{1, \dots, b\};$ and $\hat{\mathbf{U}}_{i}(w) \in \mathbb{C}^{p_{i} \times p_{i}}, \forall w \in \mathbb{C}, \forall i \in \{b + 1, \dots, b + d\}$, while $\sum_{i=1}^{b+d} p_{i} = n_{1}, p_{i} \geq 1$

• Given a constant $\tau > 0$, $\hat{U}(w)$ is included in the set

$$\mathcal{H}_{\tau} \stackrel{\triangle}{=} \left\{ \hat{\mathbf{U}}(w) \middle| \begin{array}{c} \hat{\mathbf{U}}(w) = \operatorname{diag}\left(\hat{\mathbf{U}}_{1}(w), \cdots, \hat{\mathbf{U}}_{b+d}(w)\right) \\ \hat{\mathbf{U}}(w) \in \mathcal{F}, \ \hat{\mathbf{U}}(w) \text{ is stable}, \ \|\hat{\mathbf{U}}(w)\|_{\infty} < \tau \end{array} \right\}$$

with \mathcal{F} : the set of all causal finite linear time-invariant systems

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• Controller $\hat{\mathbf{C}}(w)$ of *m*th-order is described by

Controller

$$\begin{aligned} \mathbf{x}_C(k+1) &= \mathbf{A}_C \mathbf{x}_C(k) + \mathbf{B}_C \mathbf{y}_P(k) \\ \mathbf{u}_P(k) &= \mathbf{C}_C \mathbf{x}_C(k) + \mathbf{D}_C \mathbf{y}_P(k) \end{aligned}$$

and the controller is also denoted by its parameters as

$$\mathbf{X} \stackrel{\triangle}{=} \left[\begin{array}{cc} \mathbf{D}_{C} & \mathbf{C}_{C} \\ \mathbf{B}_{C} & \mathbf{A}_{C} \end{array} \right] \in \mathbb{R}^{(s+m) \times (t+m)}$$

 X is perturbed to X + Δ due to FWL fixed-point implementation, with Δ belonging to the hypercube

$$\mathcal{D}_{\beta} \stackrel{\triangle}{=} \{ \mathbf{\Delta} \mid \mathbf{\Delta} \in \mathbb{R}^{(s+m) \times (t+m)}, \|\mathbf{\Delta}\|_{m} \leq \beta \}$$

where $0 \leq \beta \in \mathbb{R}$ is the maximum representation error, $\mathbf{\Delta} = \begin{bmatrix} \delta_{i,j} \end{bmatrix}$ and $\|\mathbf{\Delta}\|_{m} = \max_{i,j} |\delta_{i,j}|$

Closed-Loop System

Closed-loop system, which consists of P
_g(w), Û(w), X and Λ, is denoted as Φ(w, Û(w), X, Λ), where Λ is equivalent to Δ as

$$\mathbf{\Lambda} \stackrel{\triangle}{=} \operatorname{diag}(\delta_{1,1}, \delta_{2,1}, \cdots, \delta_{s+m,1}, \delta_{1,2}, \cdots, \delta_{1,t+m}, \cdots, \delta_{s+m,t+m})$$
$$\mathbf{\Lambda} \in \mathcal{O}_{\beta} \stackrel{\triangle}{=} \{\mathbf{Q} \mid \mathbf{Q} \in \mathbb{R}^{N \times N}, \mathbf{Q} \text{ is diagonal}, \bar{\sigma}(\mathbf{Q}) \leq \beta\}$$

with $\bar{\sigma}(\mathbf{Q})$ denoting the maximum singular value of \mathbf{Q}

- Further denote the closed-loop transfer function from w(k) to z(k) by Φ̂_{wz}(w, Û(w), X, Λ)
- For 0 < ξ ∈ ℝ, the set of all *m*th-order robust H_∞ controllers, which do not consider FWL effect, is defined by

$$\mathcal{X}_m \stackrel{\triangle}{=} \left\{ \mathbf{X} \left| \begin{array}{c} \mathbf{X} \in \mathbb{R}^{(s+m) \times (t+m)}, \hat{\mathbf{\Phi}}(w, \hat{\mathbf{U}}(w), \mathbf{X}, \mathbf{0}) \text{ is stable}, \\ \forall \hat{\mathbf{U}}(w) \in \mathcal{H}_{\tau}, \ \| \hat{\mathbf{\Phi}}_{wz}(w, \hat{\mathbf{U}}(w), \mathbf{X}, \mathbf{0}) \|_{\infty} \le \xi \end{array} \right. \right\}$$

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Theoretical Measure

• For a controller $\mathbf{X} \in \mathcal{X}_m$, the FWL robust measure

$$\upsilon(\mathbf{X}) \stackrel{\triangle}{=} \sup_{0 \le \beta \in \mathbb{R}} \left\{ \beta \left| \begin{array}{c} \forall \hat{\mathbf{U}}(w) \in \mathcal{H}_{\tau}, \ \hat{\mathbf{\Phi}}(w, \hat{\mathbf{U}}(w), \mathbf{X}, \mathbf{\Lambda}) \text{ is stable,} \\ \forall \mathbf{\Lambda} \in \mathcal{O}_{\beta}, \ \| \hat{\mathbf{\Phi}}_{wz}(w, \hat{\mathbf{U}}(w), \mathbf{X}, \mathbf{\Lambda}) \|_{\infty} \le \xi \end{array} \right\} \right\}$$

charaterises "robustness" of \boldsymbol{X} to controller perturbation $\boldsymbol{\Lambda}$

- \mathcal{H}_{τ} is the set of structured uncertainty
- *O*_β defines FWL perturbation hypercube
- $\hat{\Phi}(w, \hat{\mathbf{U}}(w), \mathbf{X}, \mathbf{\Lambda})$ is the whole closed-loop system
- $\hat{\Phi}_{wz}(w, \hat{U}(w), X, \Lambda)$ is the closed-loop transfer function from external perturbation input $\mathbf{w}(k)$ to controlled output $\mathbf{z}(k)$
- However, how to compute the value of v(X) is unknown
- With aid of mixed μ theorem, we derive a tractable lower bound for $v(\mathbf{X})$

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Mixed μ

"Substitute out" Û(w) from Φ̂(w, Û(w), X, Λ) ⇒ composite system of P̂_g(w), X and Λ, described by:

$$\begin{array}{lll} \mathbf{X}_{PC}(k+1) &=& \left(\overline{\mathbf{A}}(\mathbf{X}) + \mathbf{B}_{u}\mathbf{\Lambda}\mathbf{C}_{u}\right)\mathbf{X}_{PC}(k) + \mathbf{B}_{\overline{v}}\mathbf{v}(k) + \overline{\mathbf{B}}(\mathbf{X})\mathbf{w}(k) \\ \mathbf{h}(k) &=& \mathbf{C}_{\overline{h}}\mathbf{X}_{PC}(k) + \mathbf{D}_{1,1}\mathbf{v}(k) + \mathbf{D}_{1,2}\mathbf{w}(k) \\ \mathbf{z}(k) &=& \overline{\mathbf{C}}(\mathbf{X})\mathbf{x}_{PC}(k) + \mathbf{D}_{2,1}\mathbf{v}(k) + \overline{\mathbf{D}}(\mathbf{X})\mathbf{w}(k) \end{array}$$

Define the matrix

$$\begin{array}{l} \text{matrix} \\ \boldsymbol{\Theta}(\mathbf{X},\beta) \stackrel{\Delta}{=} \left[\begin{array}{ccc} \overline{\mathbf{A}}(\mathbf{X}) & \mathbf{B}_{u} & \mathbf{B}_{\overline{v}} & \overline{\mathbf{B}}(\mathbf{X}) \\ \beta \mathbf{C}_{u} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \tau \mathbf{C}_{\overline{h}} & \mathbf{0} & \tau \mathbf{D}_{1,1} & \tau \mathbf{D}_{1,2} \\ \frac{1}{\xi} \overline{\mathbf{C}}(\mathbf{X}) & \mathbf{0} & \frac{1}{\xi} \mathbf{D}_{2,1} & \frac{1}{\xi} \overline{\mathbf{D}}(\mathbf{X}) \end{array} \right]$$

and the related set of allowable perturbations \mathcal{K}_{θ}

• We can obtain a computable mixed μ : $\alpha_{\mathcal{K}_{\theta}}(\Theta(\mathbf{X},\beta))$

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Tractable Measure

- Result: ∃ 0 ≤ β ∈ ℝ such that α_{Kθ}(Θ(X, β)) < 1, then X ∈ X_m and ∀Û(w) ∈ H_τ, ∀Λ ∈ O_β
 Â(w, Û(w), X, Λ) is stable, ||Â_{wz}(w, Û(w), X, Λ)||_∞ ≤ ξ
- Define a subset of X_m as

$$\widetilde{\mathcal{X}}_{m} \stackrel{\bigtriangleup}{=} \{ \boldsymbol{\mathsf{X}} \mid \boldsymbol{\mathsf{X}} \in \mathbb{R}^{(s+m) \times (t+m)}, \alpha_{\mathcal{K}_{\theta}}(\boldsymbol{\Theta}(\boldsymbol{\mathsf{X}}, 0)) < 1 \}$$

• For
$$\mathbf{X} \in \widetilde{\mathcal{X}}_m$$
, the FWL robust measure
 $\widetilde{v}(\mathbf{X}) \stackrel{\Delta}{=} \sup_{\mathbf{0} \leq \beta \in \mathbb{R}} \{\beta \mid \alpha_{\mathcal{K}_{\theta}}(\mathbf{\Theta}(\mathbf{X}, \beta)) < 1\}$

is a lower bound of $v(\mathbf{X})$

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Design Problem

 Robust FWL controller design: given P̂_g(w), τ, ξ, m and nonempty X̃_m, find a controller X_{opt} ∈ X̃_m that achieves

$$\gamma = \sup_{\mathbf{X} \in \widetilde{\mathcal{X}}_m} \widetilde{\upsilon}(\mathbf{X})$$

- This design makes the FWL tolerance as large as possible, while satisfying a suboptimal robust control requirement
- This robust FWL controller design can be solved with aid of bilinear matrix inequality
- Complexity comparison with Yang et al. [20]
 - Our FWL robust H_{∞} controller design solves one BMI of size $2(n + m + N + n_1 + n_2)$
 - FWL robust H₂ controller design [20] requires to solve at least 2^N BMIs of size no less than 4n

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Design Problem

• Nominal plant model $\hat{\mathbf{P}}_{g}(w)$ is given by

$$\hat{\mathbf{P}}_{0}(w) = \frac{3.3750 \times 10^{-3}w + 1.3669 \times 10^{-2}w^{2} + 3.4605 \times 10^{-3}w^{3}}{1 - 3.0488w + 3.1001w^{2} - 1.0513w^{3}},$$

$$\hat{\mathbf{W}}_{1}(w) = \frac{4.9875 \times 10^{-3} w}{1 - 9.9501 \times 10^{-1} w}, \ \hat{\mathbf{W}}_{2}(w) = \frac{5.8512 \times 10^{-1} w - 5.5933 \times 10^{-1} w^{2}}{1 - 1.3390 w + 3.7908 \times 10^{-1} w^{2}}$$

• Plant model uncertainty $\hat{\mathbf{U}}(w) \in \mathcal{H}_{\tau}$ with $\tau = 0.4$



Design Solution

- Constant that bounds closed-loop H_{∞} norm from **w** to **z** was set to $\xi = 0.3$, and controller order was chosen to be m = 2
- Solving optimal FWL robust design problem yields the controller

$$\mathbf{X}_{\text{opt1}} = \begin{bmatrix} -103.44 & -15.600 & -1.4984 \\ \hline -16.070 & -1.4261 & 0.25055 \\ -19.469 & -3.0400 & 0.37517 \end{bmatrix}$$

with $\widetilde{\upsilon}(\boldsymbol{X}_{opt1}) = 8.2842 \times 10^{-3}$

- For any FWL perturbation to \mathbf{X}_{opt1} smaller than 8.2842×10^{-3} and for any $\hat{\mathbf{U}}(w) \in \mathcal{H}_{\tau}$ with $\tau = 0.4$,
 - the closed-loop system maintains stability, and
 - closed-loop ${\rm H}_\infty$ norm from ${\boldsymbol w}$ to ${\boldsymbol z}$ is always less than 0.3

Bit Length Estimate

- Using fixed point processor of *c*-bit length to implement X, *c* bits are assigned as:
 - 1 sign bit, *c*_{int} bits for integer part, *c*_{fra} bits for fraction part
- To guarantee dynamic range of **X**, $c_{int} = \lceil \log_2 \|\mathbf{X}\|_m \rceil$,
- Fraction bit length bounds the absolute values of FWL errors by $2^{-(c_{fra}+1)}$, and to maintain closed-loop performance, at least

$$c_{fra} = \left\lceil -\log_2 \widetilde{v}(\mathbf{X}) \right\rceil - 1$$

• Minimal bit length guaranteeing closed-loop performance, estimated based on $\tilde{v}(\mathbf{X})$, is

$$\widetilde{c}(\mathbf{X}) \stackrel{ riangle}{=} \lceil \log_2 \|\mathbf{X}\|_m \rceil + \lceil -\log_2 \widetilde{v}(\mathbf{X}) \rceil$$

In this example, $\tilde{c}(\mathbf{X}_{opt1}) = 14$

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Design Problem

- Example from Yang et al. [20] was for FWL H₂ control under plant parameter uncertainty
- Noting $\|\hat{\Phi}_{wz}\|_{\infty} \ge \|\hat{\Phi}_{wz}\|_2$ and structured uncertainty includes parameter uncertainty, we substituted $\|\hat{\Phi}_{wz}\|_{\infty}$ for $\|\hat{\Phi}_{wz}\|_{2}$ and plant structured uncertainty for plant parameter uncertainty
- Nominal plant model $\hat{\mathbf{P}}_{q}(w)$ is defined by

$$\mathbf{A}_{P} = \begin{bmatrix} 0.5 & 0.1 \\ 0.2 & 0 \end{bmatrix}, \ \mathbf{B}_{V} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \ \mathbf{B}_{W} = \begin{bmatrix} 1 & 0 \\ 1 & 0 \end{bmatrix}, \ \mathbf{B}_{P} = \begin{bmatrix} 1 \\ 0 \end{bmatrix},$$
$$\mathbf{C}_{h} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}, \ \mathbf{C}_{Z} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}, \ \mathbf{D}_{2,2} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \ \mathbf{D}_{2,3} = \begin{bmatrix} 1 \\ 1 \end{bmatrix},$$
$$\mathbf{C}_{P} = \begin{bmatrix} 0 & -1 \end{bmatrix}, \ \mathbf{D}_{3,2} = \begin{bmatrix} 1 & 1 \end{bmatrix}, \ \mathbf{D}_{1,1} = \mathbf{D}_{1,2} = \mathbf{D}_{2,1} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

Plant structure uncertainty is defined by

$$\hat{\mathbf{U}}(w) = \varphi(w) \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \in \mathcal{H}_{\tau} \text{ with } \varphi(w) \in \mathbb{C} \text{ and } \tau = 0.13$$

Design Solution

 Set constant ξ = 4.9676. We designed 1st-order controller by solving the FWL robust design problem, leading to

$$\mathbf{X}_{\text{opt2}} = \begin{bmatrix} 1.0853 & -0.36600 \\ \hline 1.1031 & -0.34734 \end{bmatrix}$$

with $\tilde{v}(\mathbf{X}_{opt2}) = 0.0275$, which can be implemented with a fixed point processor of $\tilde{c}(\mathbf{X}_{opt2}) = 7$ bits

- As ||Φ̂_{wz}||_∞ ≥ ||Φ̂_{wz}||₂, system was guaranteed to be closed-loop stable and ||Φ̂_{wz}||₂ < 4.9676 when τ = 0.13 and the FWL bound was 0.0275
- Yang *et al.* [20] obtained a controller achieving $\|\hat{\Phi}_{wz}\|_2 < 3.0822$ when $\tau = 0.13$ and the FWL bound 0.0275
- Our method required to solve one BMI of size 22, while Yang *et al.* [20] required to solve 32 BMIs of size 8

Conclusions

We have used mixed μ theory to directly design optimal robust FWL controllers, and our novel contributions include:

- A robust FWL control performance measure taking into account both robust control requirements and FWL implementation considerations
- This robust FWL control performance measure can be computed conveniently using LMI
- Optimal robust FWL controller design is formulated as a mixed µ problem, which can be solved by means of BMI

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